# **Goal-Oriented Anisotropic Mesh Adaptation in the SU2 Framework**

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## Overview

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- Conclusions and future work



### **Motivation**

- Accuracy and robustness of high-fidelity analysis and design are highly dependent on discretization
- Mesh generation is a significant bottleneck in the CFD workflow [CFD Vision 2030]
- Physical phenomena are highly anisotropic in nature







### Previous work

- Grid adaptation for functional outputs using an *a posteriori* error estimate [Venditti and Darmofal, 2000]
- Development of a priori interpolation error estimates [Formaggia and Perotto, 2001]
- Continuous mesh framework with optimal metric for error control in L<sup>p</sup>-norm [Alauzet et al., 2006]
- A priori functional error estimate for 3D Euler equations and Spalart-Allmaras [Loseille et al., 2010], [Frazza, 2018]

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## Previous work in SU2

Isotropic adaptation

[Palacios et al., 2012], [Copeland et al., 2013]

- > Gradients
- > Adjoint-weighted residuals
- Feature-based anisotropic adaptation [Loseille et al., 2016]
- Goal-oriented adaptation for Euler equations and TNE2 [Munguía et al., 2020]
  - Adjoint-weighted error in fluxes and chemical source terms





### Feature-based vs goal-oriented adaptation

#### Feature-based

Best mesh to compute characteristics of a solution  $\boldsymbol{u}$ 



 $\|u-\Pi_h u\|_{L^p(\Omega_h)}$ 

#### **Goal-oriented**

Best mesh to compute a functional f(u)



 $\|f(u) - f(\Pi_h u)\|_{L^p(\Omega_h)}$ Stanford University



### Metric space

- Linear elements → second-order interpolation error
- Riemannian metric space given by Hessians, e.g. in 2D:

$$\mathcal{M}(\boldsymbol{x}) = \begin{bmatrix} u_{xx} & u_{xy} \\ u_{yx} & u_{yy} \end{bmatrix} = \begin{bmatrix} a & b \\ b & c \end{bmatrix}$$

• Edge length in Euclidean metric space (i.e.  $\mathcal{M}$  constant in space):

$$l_{\mathcal{M}}^{2} = \vec{s}^{T} \mathcal{M} \vec{s} h^{2} = (ax^{2} + 2bxy + cy^{2})h^{2}$$
$$\mathcal{M} = \mathcal{R} \begin{bmatrix} 1/h_{1}^{2} & 0\\ 0 & 1/h_{2}^{2} \end{bmatrix} \mathcal{R}^{T}$$

Edge length in Riemannian metric space:



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**Discrete-continuous duality** 

DiscreteElement KElement volume |K|Mesh X of  $\Omega_h$ Number of vertices N

ContinuousMetric tensor  $\mathcal{M}$  $d^{-1} = \sqrt{\det \mathcal{M}(x)}$ Riemannian metric space  $\mathbf{M} = \mathcal{M}(x)$  of  $\Omega$ Complexity  $\mathcal{C}(\mathbf{M}) = \int_{\Omega} \sqrt{\det \mathcal{M}(x)} d\Omega = \mathcal{N}$ 



### **Optimal metric**

Minimize error in L<sup>p</sup>-norm for problem of dimension d:

$$\mathcal{M}_{\mathbf{L}^{p}} = \mathcal{N}^{\frac{2}{d}} \left( \int_{\Omega} (\det|\mathcal{H}(\mathbf{x})|)^{\frac{p}{2p+d}} d\Omega \right)^{-\frac{2}{d}} (\det|\mathcal{H}(\mathbf{x})|)^{-\frac{1}{2p+d}} |\mathcal{H}(\mathbf{x})|$$

- 1. Desired complexity
- 2. Global normalization
- 3. Local normalization

Free parameters:  $\mathcal{N}$  and p

### **Optimal metric**

- Choice of p dictated by problem
  - > Larger p damps small amplitude variations
  - > Previous work suggests p = 1,2 for Euler, p = 4 for RANS [Frazza, 2018]



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p = 4

### Inviscid error estimate

- For Euler equations, can approximate error using flux and source differencing:  $R(u) = \nabla \cdot F(u) - Q(u) = 0$   $\delta f \approx \int_{\Omega_h} \bar{u}^T [ (\nabla \cdot F_h(u) - \nabla \cdot F(u)) - (Q_h(u) - Q(u)) ] d\Omega_h$
- Integrating by parts and neglecting boundary terms:

$$\delta f \approx \int_{\Omega_{h}} \left[ \nabla \bar{u}^{T} \left( F(u) - F_{h}(u) \right) + \bar{u}^{T} \left( Q(u) - Q_{h}(u) \right) \right] \mathrm{d}\Omega_{h}$$

Adjoint-weighted Hessian:

$$\mathcal{H}(\boldsymbol{x}) = \left| \frac{\partial \bar{u}_j}{\partial x_i} \right| \left| H\left( F_i(u_j) \right) \right| + \left| \bar{u}_j \right| \left| H\left( Q(u_j) \right) \right|$$

OK results for Euler and TNE2, but doesn't properly weigh errors due to gradients

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### Viscous error estimate

Approximate error by linearizing wrt conservative variables

$$\delta f \approx \int_{\Omega_h} \bar{u}^{\mathrm{T}} \frac{\partial R}{\partial u} (u - u_h) \mathrm{d}\Omega_h$$

First we need to manipulate terms of the following forms:

$$(w\bar{u})^T (u - u_h)$$
 Zeroth-order  
e.g. source terms

$$(w\bar{u})^T \frac{\partial(u-u_h)}{\partial x_i}$$

First-order e.g. convective terms

$$(w\bar{u})^T \frac{\partial^2 (u-u_h)}{\partial x_i \partial x_j}$$

Second-order e.g. viscous terms

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### Viscous error estimate

Neglecting boundary terms, we obtain the following form for viscous terms:

$$\int_{\Omega} (w\bar{u})^T \frac{\partial^2 (u - u_h)}{\partial x_i \partial x_j} d\Omega \approx \int_{\Omega} \left( w \frac{\partial^2 \bar{u}}{\partial x_i \partial x_j} \right)^T (u - u_h) d\Omega$$

- Weights w obtained by linearizing governing equations
- E.g. second-order energy error due to divergence of heat flux

$$\nabla^2 T = \frac{1}{\rho c_v} \left[ \nabla^2 (\rho c_v T) - c_v T \nabla^2 \rho \right]$$
$$\overline{H}_{\rho e} = -\frac{\lambda + \lambda_t}{\rho c_v} \left[ \left( \overline{u}_{\rho e} \right)_{xx} + \left( \overline{u}_{\rho e} \right)_{yy} + \left( \overline{u}_{\rho e} \right)_{zz} \right]$$

Adjoint-weighted Hessian:

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 $\mathcal{H}(\boldsymbol{x}) = (|\bar{C}_k| + |\bar{G}_k| + |\bar{H}_k|)|H(u_k)|$ 

### Simplification for SST error estimate

Treat blending functions as constant

$$\phi = F_1 \phi_1 + (1 - F_1) \phi_1$$

$$F_1 = \tanh(arg_1^4), F_2 = \tanh(arg_2^2)$$

$$arg_1 = \min\left[\max\left(\frac{\sqrt{k}}{\beta^*\omega d}, \frac{500\nu}{d^2\omega}\right), \frac{4\rho\sigma_{\omega 2}k}{CD_{k\omega}d^2}\right]$$

$$arg_2 = \max\left(\frac{2\sqrt{k}}{\beta^*\omega d}, \frac{500\nu}{d^2\omega}\right)$$

Don't limit shear stress or production

$$\mu_{t} = \frac{\rho k a_{1}}{\max(\omega a_{1}, \Omega F_{1})}$$
$$P_{k} = \max\left(\tau_{t,ij} \frac{\partial u_{i}}{\partial x_{j}}, 20\beta^{*}\rho k\omega\right)$$

Linearize all other terms, including viscosity and thermal conductivity

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### Modifications to NS and SST solver

- Store conservative turbulent variables
  - > Adjoints in master/develop obtained wrt turbulent primitives
  - > Error estimate in terms of conservative primal and adjoint variables
- Replace solution clipping with under-relaxation
- Remove  $\omega$  production limiter

$$P_{\omega} = \frac{\gamma}{\nu_t} \tau_{t,ij} \frac{\partial u_i}{\partial x_j}$$



## Modifications to NS and SST solver

• Use wall distance instead of "normal neighbor" distance in  $\omega$  wall BC

$$\omega_{wall} = \frac{60V}{\beta_1 (\Delta d_1)^2}$$

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- Use over-relaxed gradient correction
  - > More stable on highly non-orthogonal meshes [Jasak, 1996]
- Include Jacobians of
  - > Green-Gauss gradients
  - > Production and cross-diffusion
  - > Laminar and eddy viscosity

			1	
0	0.026851	0.053701	0.080552	0.1074
		56547		
				10105



### Adaptation framework

- SU2: Flow, adjoint, and metric computation
- AMGIO: Conversion to and from GMF
- pyAMG: Mesh adaptation and solution interpolation
- "Stable" branch: feature\_adap



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## Running SU2-AMG

- Currently limited to tri and tet meshes
- Background surface mesh
  - > Fine representation of surface
  - > SU2 or GMF
  - > Defaults to initial mesh
- Ridge detection
  - Let AMG detect edges (3D) and corners (2D)
  - python script to append corners based on intersection of markers

```
PYADAP BACK= rae2822 fine.su2
```

```
PYADAP_RDG= NO
```

```
$ set_corner_points.py -f rae2822_rans.su2
NCORNERS= 2
1 0
1 512
```

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## Running SU2-AMG

- Adaptation type
  - > Goal, Mach, or pressure
- Target complexity
- Iterations per mesh level
- Norm

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PYADAP\_COMPLEXITY= (30000, 60000, 120000)
PYADAP\_SUBITE= (5, 5, 5)
PYADAP\_NORM= 2.0

PYADAP\_SENSOR= GOAL % MACH, PRES



## Running SU2-AMG

- Maximum cell size
- Minimum cell size
  - > Very important for RANS
- Gradation parameter
  - > Max ratio of neighboring cell sizes



 $h_{grad} = 1.5$ 

- PYADAP\_HMAX= 500.0 PYADAP HMIN= 1.0E-6
- PYADAP\_HGRAD= 3.0



 $h_{grad} = 3.0$  Stanford University



### RAE 2822

- *M* = 0.729
- $Re = 6.5 \times 10^6$
- *α* = 2.31°
- $f = c_l$
- *N* = 30000, 60000, 120000, 240000
- $h_{min} = 1.0 \times 10^{-6}$
- $h_{max} = 500$
- $h_{grad} = 3.0$



Initial mesh: 29996 points

### RAE 2822



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RAE 2822 (*p* = 2)



### Final mesh: 83687 points

 $c_p$ 

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RAE 2822 (*p* = 2)



### Final mesh: 83687 points

Mach number

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RAE 2822 (*p* = 2)



### Final mesh: 83687 points

Mach number

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### Conclusions

- Implemented error estimate and goal-oriented mesh adaptation
  - > Euler
  - > TNE2 [Munguía et al., 2020]
  - > SST
- Demonstrated ability to properly adapt for viscous, turbulent flows on RAE 2822
- Modifications to SST solver seem to have improved robustness on nonorthogonal meshes



### Future work

Thorough investigation of effects of adaptation parameters

- > Norm
- Gradation
- Implement error estimates for other models
  - Spalart-Allmaras
  - Incompressible
  - > Wall functions
- CAD-based projection
- Mesh-adaptive shape optimization

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