

# EFFECT OF ROUGHNESS ON WIND TURBINE PERFORMANCE

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- > Leading edge erosion
- > Modeling effect of erosion
- Validation against theory
- ) Airfoil results
- > Turbine performance analysis
- > Future work

### **LEADING EDGE EROSION**

- > Due to rain, hail, insects ...
- ) Offshore locations more vulnerable
- > Leads to reduction in performance
- > Eroded blades modeled as rough surfaces



Image from <a href="https://www.grow-offshorewind.nl/project/windcore#modalTrigger1">https://www.grow-offshorewind.nl/project/windcore#modalTrigger1</a>

### **MODELING EFFECT OF EROSION**

- > Extent of erosion represented by *roughness height k*.
- ) RANS turbulence models based on *equivalent sand grain roughness*  $k_s$  derived from k.
- ) Different roughness regimes identified based on  $k_s^+$ :
  - ▶  $k_s^+ \leq 5$ , *Hydraulically smooth* no effect
  - >  $5 \le k_s^+ \le 70$ , **Transitionally rough** shift in velocity profile in the inner boundary layer
  - >  $k_s^+ \ge 70$ , *Fully rough* No viscous sublayer



Image from Schlichting, H., & Gersten, K. (2016). *Boundary-layer theory*. Springer.

# **RANS MODELS FOR ROUGH WALLS**

Shift in velocity profile modeled as

### SA

- > Assume a virtual wall exists above the rough surface.
- > Non -zero turbulent viscosity at the wall to account for the shift.

$$\left. \frac{\partial \tilde{v}}{\partial n} \right|_{w} = \frac{\tilde{v}_{w}}{0.03k_{s}}$$

) Wall distance modified as  $d_{new} = d + 0.03k_s$ 

### SST

) Reduce damping in the inner boundary layer by modifying  $\omega$  at the wall.

$$\omega_w = \frac{\mu^2 S_R}{\nu}$$

)  $S_R$  is a function of  $k_s^+$ 

### **ROUGHNESS MODELS IN SU2**

> Currently implemented in branch feature\_roughwall (pull request under review).

WIP Rough wall boundary condition for SA and SST turbulence models. #877

> Choose the rough and smooth parts of airfoil separately



) Specify sand grain roughness  $(k_s)$  in config file (input method under review)

• 6 Navier-Stokes wall boundary marker(s) (NONE = no marker) MARKER\_HEATFLUX= ( airfoil, 0.0, airfoil\_rough, 0.0) WALL\_TYPE= SMOOTH, ROUGH WALL\_ROUGHNESS= 0.0, 0.000154 WALL\_ROUGHNESS= 0.0, 0.000308

## **FLOW OVER ROUGH FLAT PLATE**

- )  $Re = 6 \times 10^6$ .
- > Velocity profiles in the viscous sub layer and log law region compared to theoretical predictions



### NACA 652215 AIRFOIL

> NACA 652215 airfoil – sharp trailing edge.

- )  $k_s/c = 154 \times 10^{-6}$  ,  $k_s/c = 308 \times 10^{-6}$  at  $Re = 2.6 \times 10^{6}$
- > Roughness span  $-0.15 \le \frac{x}{c} \le 1$  (entire upper surface and part of lower surface)





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### WIND TURBINE PERFORMANCE - AVATAR

- > AVATAR turbine 10 MW reference blade (https://www.eera-avatar.eu/home/index.html)
- > Rotor blade made up of 5 airfoil sections DU240, DU300, DU350, DU400, DU600.
- Use polars generated from CFD in combination with Blade Element Momentum (BEM) to compute power output.



#### Home Why this project? Work structure News Extranet Contact Consortium Results and deliverables

#### What is AVATAR?

AVATAR is a project initiated by the European Energy Research Alliance (EERA), carried out under the FP7 program of the European Union. Its main goal is the development and validation of advanced aerodynamic models, to be used in integral design codes for the next generation of large scale wind turbines (up to 20MW).



Latest news

#### Workshop Innovations for LCOE reduction in offshore wind energy technologies, models and strategies

#### Final AVATAR consortium meeting at TU Delft

October 17, 2017 – On 25, 26, 27 October the AVATAR final consortium meeting will take place at TU Delft. ►

#### Presentation at Wind Energy

Science Conference 2017 July 3, 2017 – 26 June - 29 June Gerard Schepers (ECN) gave a presentation at the Wind Energy Science Conference 2017 at DTU ... >

#### AVATAR consortium meeting at CENER

April 6, 2017 – On 3, 4 and 5 April 2017, the 8th plenary progress meeting was held at CENER. Most of the discussion took place on ... ►

Progress meeting at NTUA in Athens December 1, 2016 – On 28, 29 and 30

## WIND TURBINE PERFORMANCE - AIRFOIL POLARS

- )  $Re = 2 \times 10^{6}$
- > Decrease in aerodynamic efficiency with roughness.
- > Span of roughness has significant impact.





## WIND TURBINE PERFORMANCE - AVATAR

- > Only SA model used here since better performance was observed.
- ) Fully turbulent conditions assumed, incoming velocity of 10 m/s.
- Assume rough sections on the LE ( $\frac{x}{c} \le \pm 0.015$ ) of DU300 and DU350 ( $k_s = 600 \times 10^{-6}$ ).
- Blade Optimization Tool (BOT) based on Blade Element Momentum theory used to compute power output

	Power (kW)	Loss (%)
Clean	8296	-
Rough DU300	8177	1.4
Rough DU350	8215	0.9
Both Rough	8089	2.4

Power output under various conditions.

# **FUTURE WORK**

- ) More validation,
- > Transition modelling ,
- > Corrections to the SST roughness models,
- > Power analysis at different roughness levels,
- > Full 3-D RANS analysis on turbine blade with real roughness.

# THANK YOU FOR YOUR TIME

